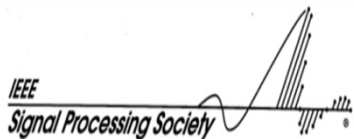


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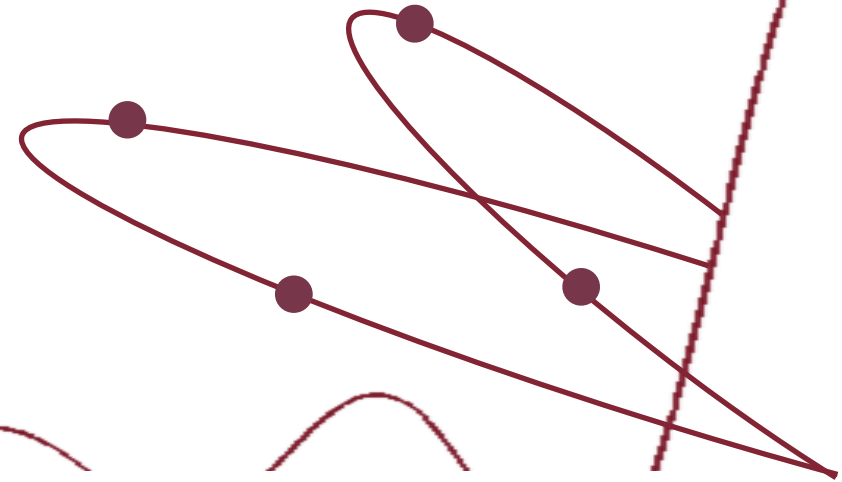
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DIRECTION OF ARRIVAL ESTIMATION USING A CLUSTER OF BEAMS IN A CONE-SHAPED DIGITAL ARRAY RADAR



DEPARTMENT OF
INFORMATION ENGINEERING,
ELECTRONICS AND TELECOMMUNICATIONS



SAPIENZA
UNIVERSITÀ DI ROMA



FINCANTIERI
The sea ahead

Sensor Signal Processing for Defence SSPD Conference 2015

Edinburgh, 9-10 September 2015

Micaela Contu, Marta Bucciarelli, Pierfrancesco Lombardo,
Francesco Madia, Rossella Stallone, Marco Massardo

Outline

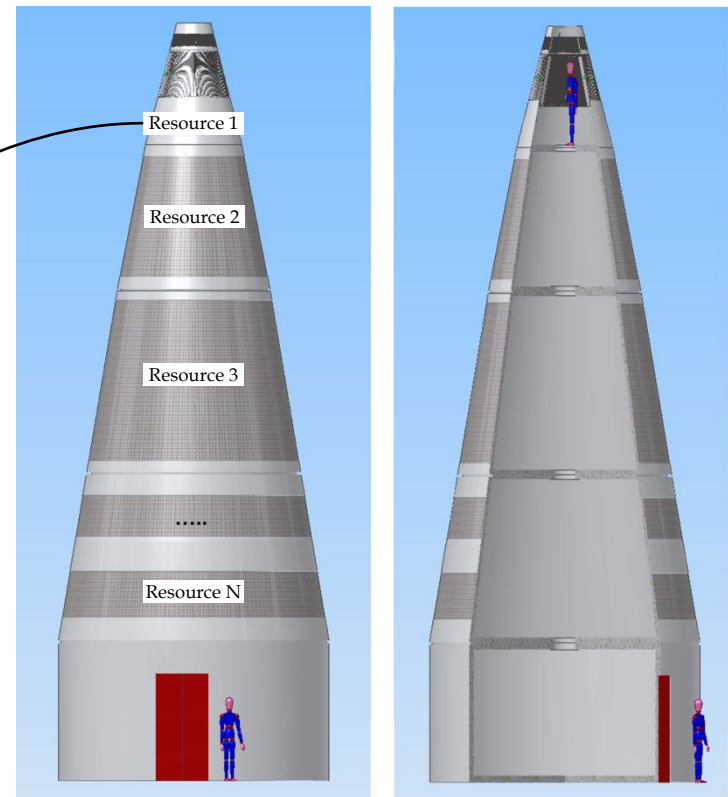
- System description and potentialities
- PAR vs DAR with conical array
- Aim of the study
- Proposed direction of arrival estimation technique
- Cramer Rao lower Bound derivation for elevation direction of arrival estimation
- Cramer Rao lower Bound comparison
- Beam cluster tilt
- Conclusions

System description (1/2)

- Innovative architecture for masts to be mounted on ships “d.Mast”, which is being studied and demonstrated by Fincantieri S.p.A. and Seastema S.p.A.
- N available resources
- Conical geometry
- Shared services

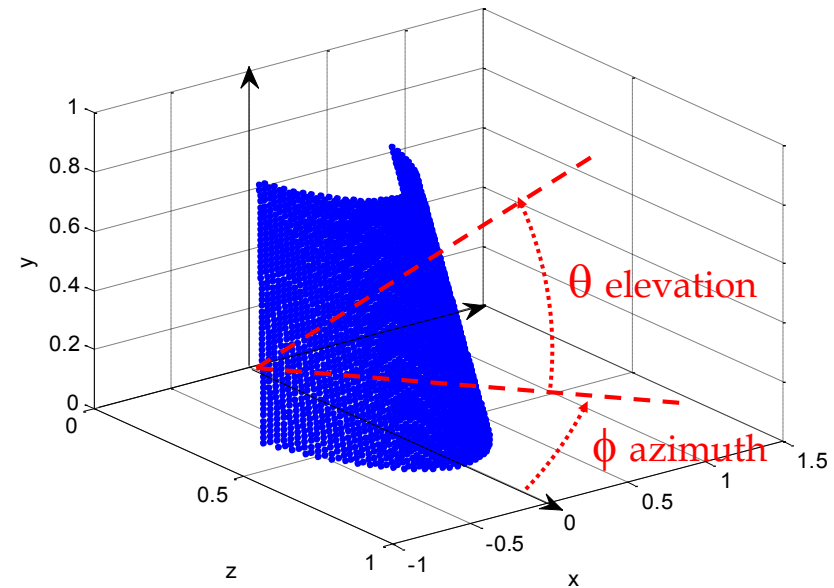
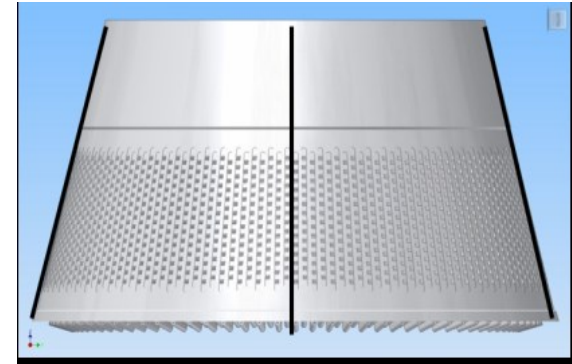
↓
Technological
breakthrough

X-band Radar is one of
the available resources



System description (2/2)

- The RX array is modelled as the “d.Radar”
- Conical array whose horizontal sections have the same number of radiating elements.
- Approximate dimensions
 - Larger diameter less than 1,5 m
 - Height less than 1 m
- AD conversion at element level.

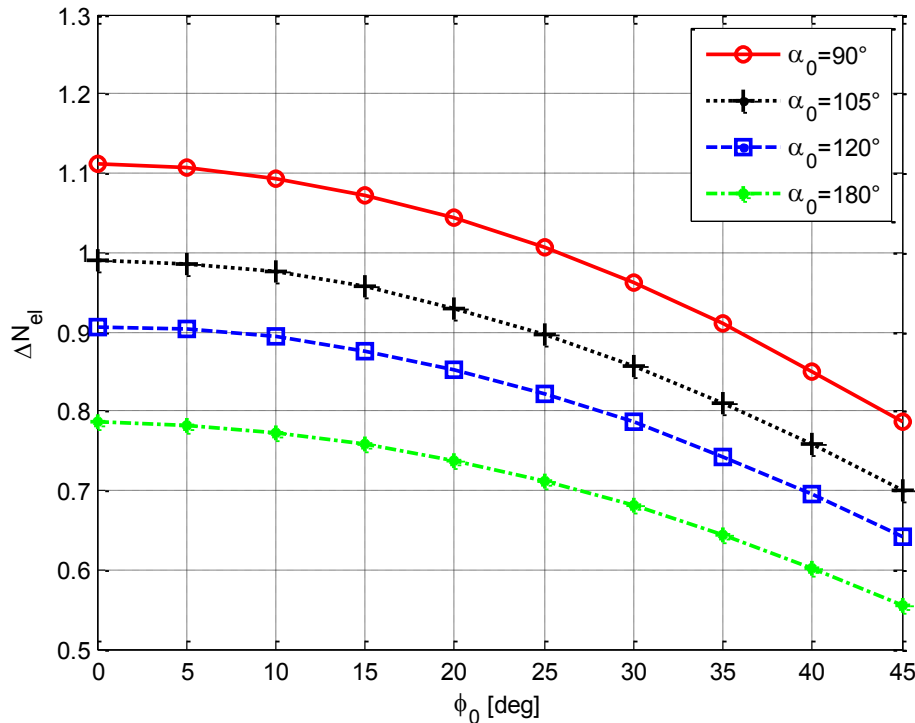
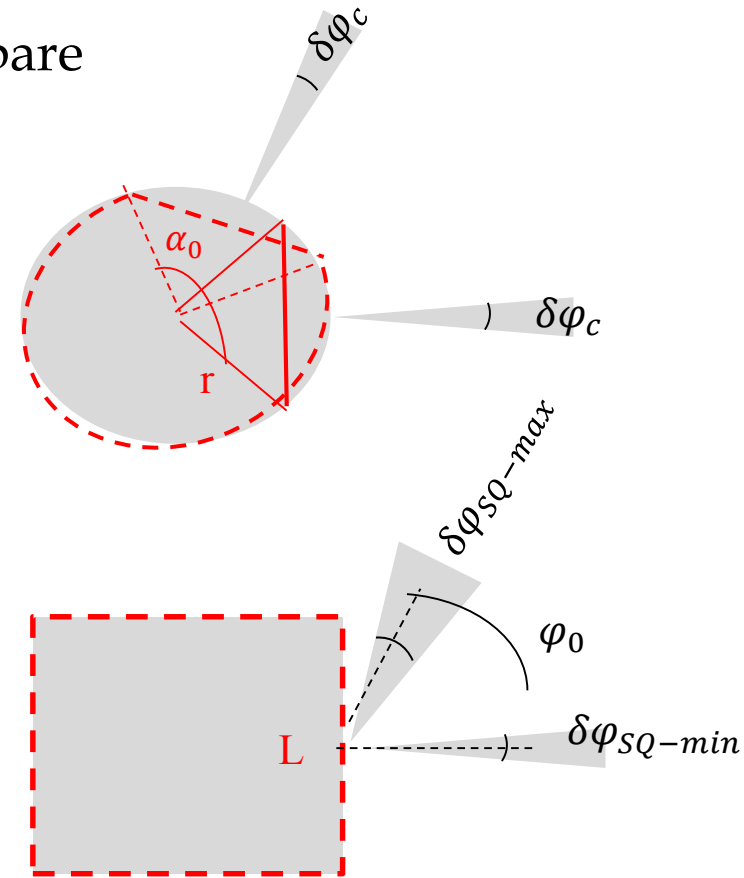


Circular array & number of radiating elements

■ The circular shape of the array allows to spare radiating element

■ Rule of thumb

$$\Delta N_{el} = \frac{N_{el}(circ)}{N_{el}(square)} = \frac{2\pi r}{4L} = \frac{\pi \cos(\varphi_0)}{4 \sin(\alpha_0/2)}$$



Compare performance of the different array configurations in the worst case ($\delta\varphi_{SQ-max}$)

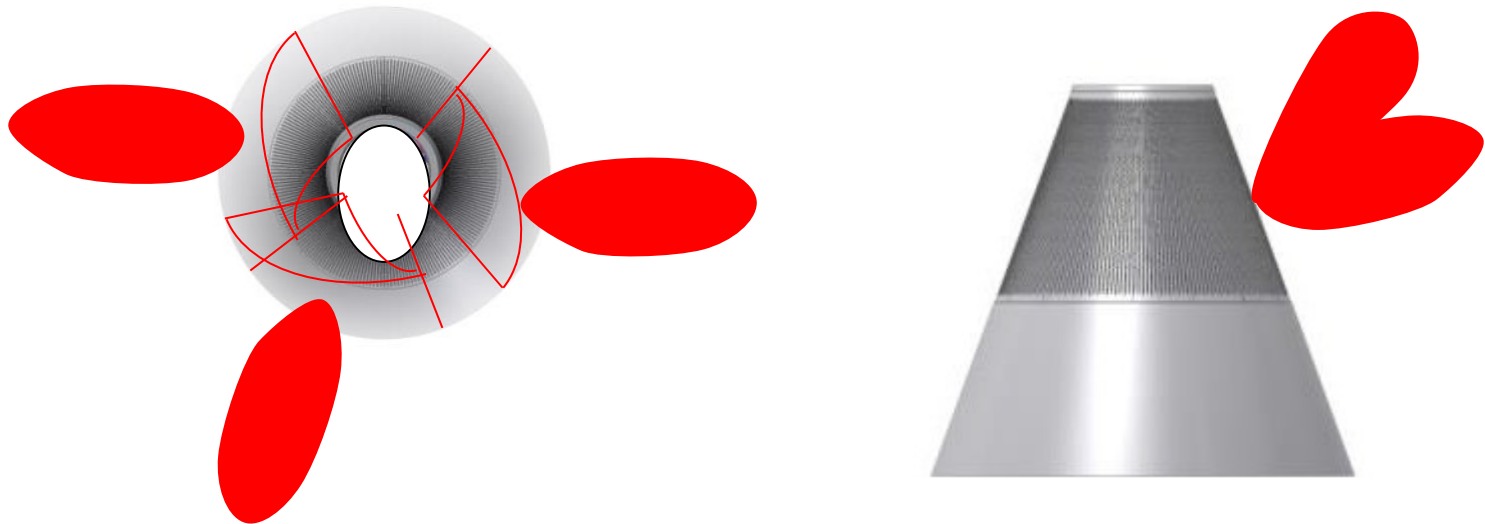
Circular array & 3D angular scan/coverage

- 360° azimuth beamforming without beamsteering, only shifting of the sector of active elements



Beams have the same width in azimuth whichever the steering direction is!

- Coverage in elevation with traditional beamforming.



PAR vs DAR for circular-based array

Array of radiating elements to form multiple beams with different characteristics and functionalities

■ Phased Array Radar (PAR)

Analog BeamForming (ABF) through beamforming networks

- ❑ fixed number of beams
- ❑ pre-determined beam characteristics

■ Digital Array Radar (DAR)

Early analog to digital (AD) conversion at and recording of all the amount of data for successive centralized processing

- ❑ “Ubiquitous radar”
- ❑ reduction of the dynamic range and isolation requirements
- ❑ **Natural solution with circular array**

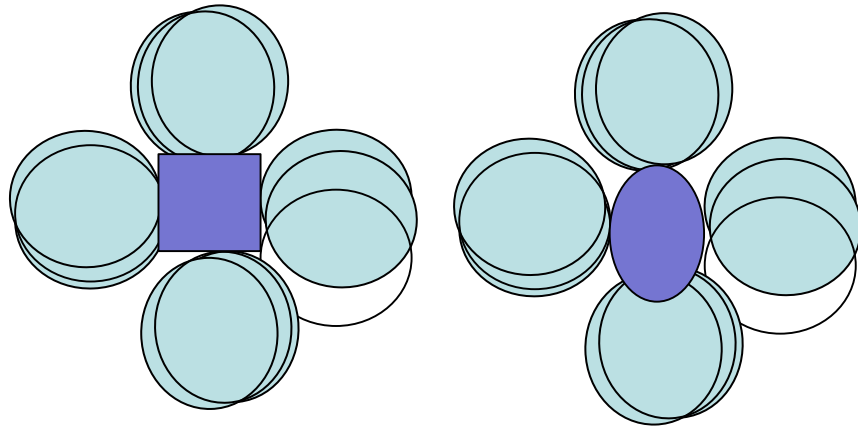
DAR provides flexibility at the expense of increased computational load and data transfer rate

advanced processing schemes are required to improve efficiency

Digital vs Phased Array Radar (I)

Phased Array

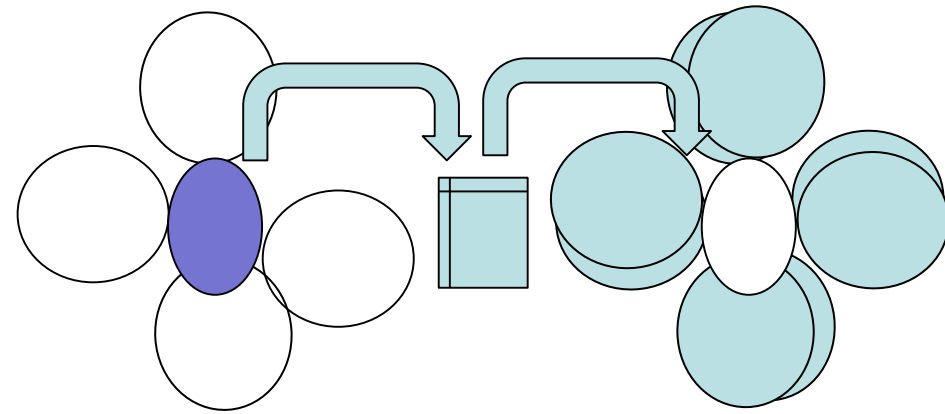
- Fixed number of beams (BFN)
- Beam shape is fixed at design time



- RX beam are necessarily always present for:
 - Detection
 - DoA estimation (otherwise DoA of detection must be illuminated again)

Digital Array

- Fixed number of beams given by the maximum available computational load
- It is possible to synthesize virtually any desired beam by storing the data collected at the element level



- It is possible to modify beams adaptively depending on data content
- Δ monopulse beams can be evaluated only for the «range cells» where a target has been detected

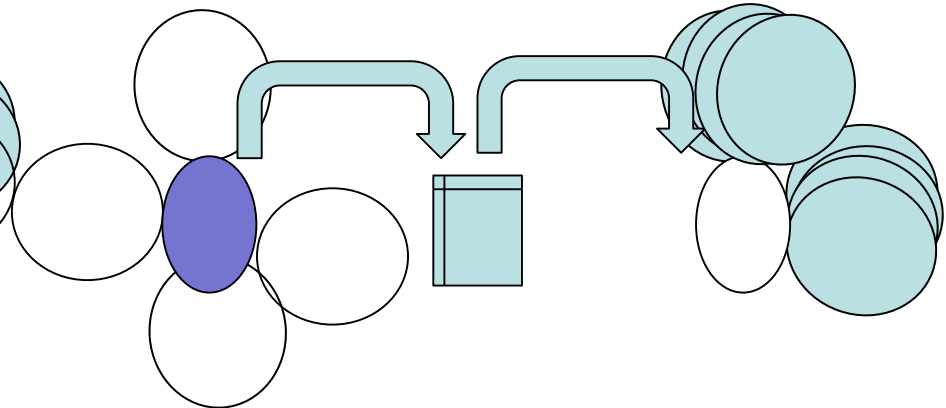
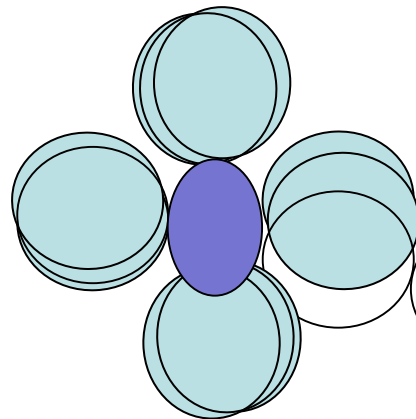
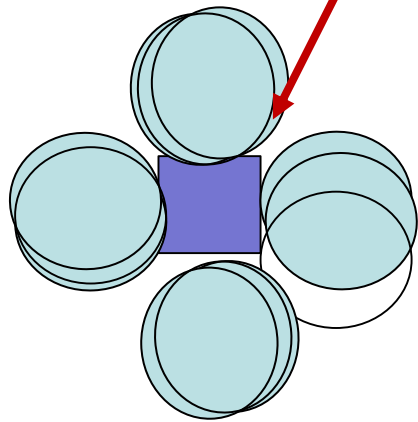
Digital vs Phased Array Radar (II)



Flexibility in the use of multiple beams

Phased Array

- Beam cluster with preassigned shape



Digital Array

- Few beams are used for the search
- It is possible to add beams in «critical» regions, use multiple tilts to handle clutter, etc...
- A lot of computation capability is left for accurate DoA estimation, corrections, etc..

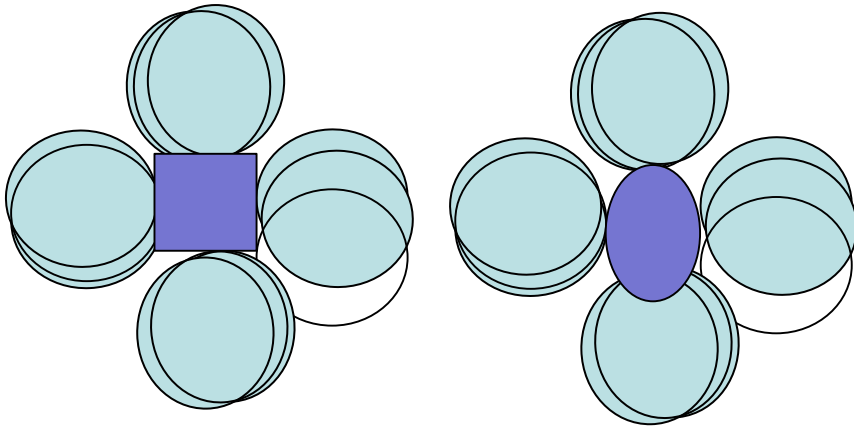
Digital vs Phased Array Radar (III)

Stima DOA interferenti CW (i.e. standoff jammer)

- Inhibit TX for a some PRTs and collect responses
- How many times TX must be inhibited to know the whole intereference scenario?

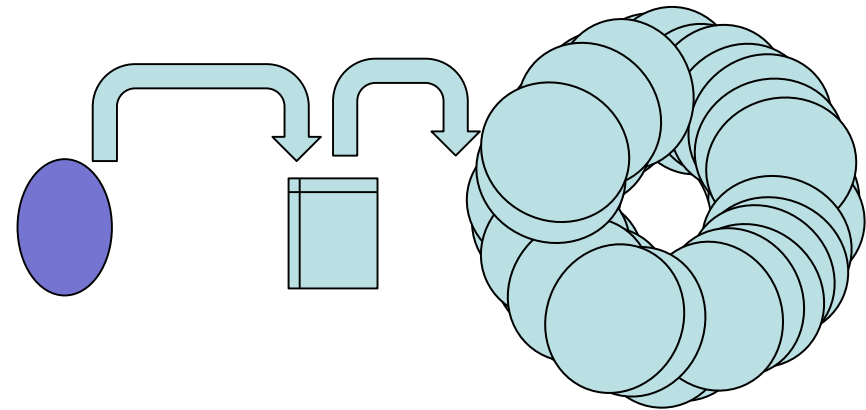
Phased Array

- For each inhibited TX, a few DoAs are suveryed, covered by the avaibalble RX beam cluster
- Many inhibited PRTs are necessary to cover all angles



Digital Array

- With a single inhibited PRT data rom all DoAs are collected
- Then beams in all directions can be synthesized in background



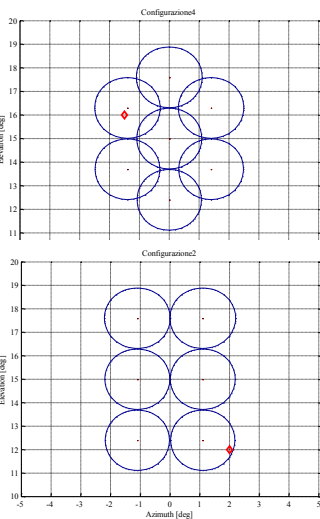
Digital vs Phased Array Radar (IV)

CW interference nulling (i.e. standoff jammer)

- Beam cluster use

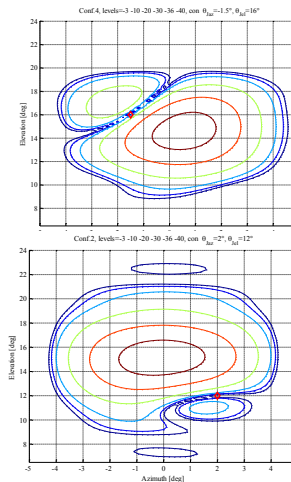
Phased Array

- Performance depends on the used beam cluster
- Beam cluster optimisation to cancel MB jammer and estimate target DoA



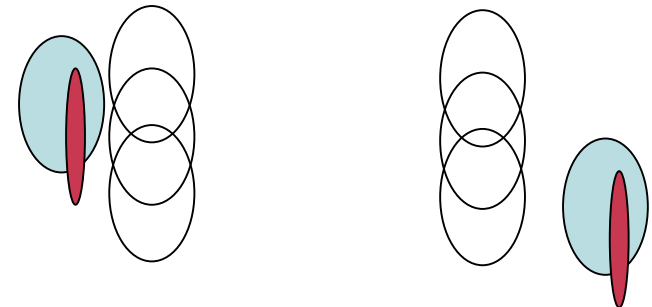
7 Fasci Σ con
puntamenti $(\theta_{az}, \theta_{el}) =$
(0, 13.4); (-1.4, 14.7);
(1.4, 14.7); (0, 15)
(-1.4, 16.3); (1.4, 16.3)
(0, 17.6)

6 Fasci Σ con
puntamenti $(\theta_{az}, \theta_{el}) =$
(-1.1, 13.4); (1.1, 13.4)
(-1.1, 17.6); (1.1, 17.6)
(-1.1, 15); (1.1, 15)



Digital Array

- After jammer DoA estimation, it is possible to build a beam steered to it
- Close-to-ideal performance achievable
- Use of single auxiliary beam to cancel jammer - reduced adaptivity losses



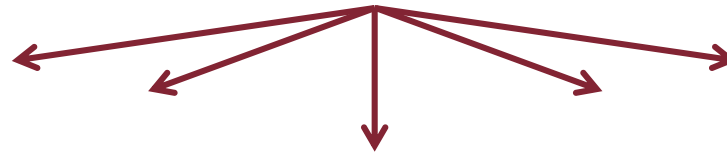
Aim of the study



Starting point: innovative conformal DAR system



Numerous potentialities



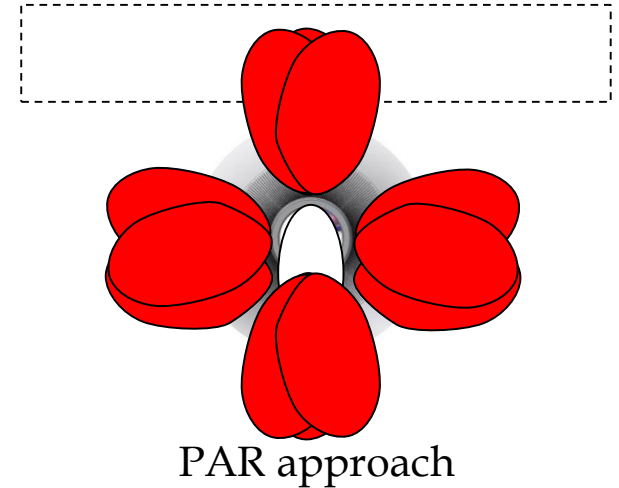
Analysis of an approach for
Direction of Arrival (DoA) estimation based on a
properly designed crowded cluster of RX beams and
comparison with traditional
monopulse approach



PAR vs DAR multiple beam forming

■ Typical cluster of beams in PAR:

- for each azimuthal direction and range
 N_{Σ} sum beams, N_{Δ} difference beams
+ 1 omnidirectional beam.



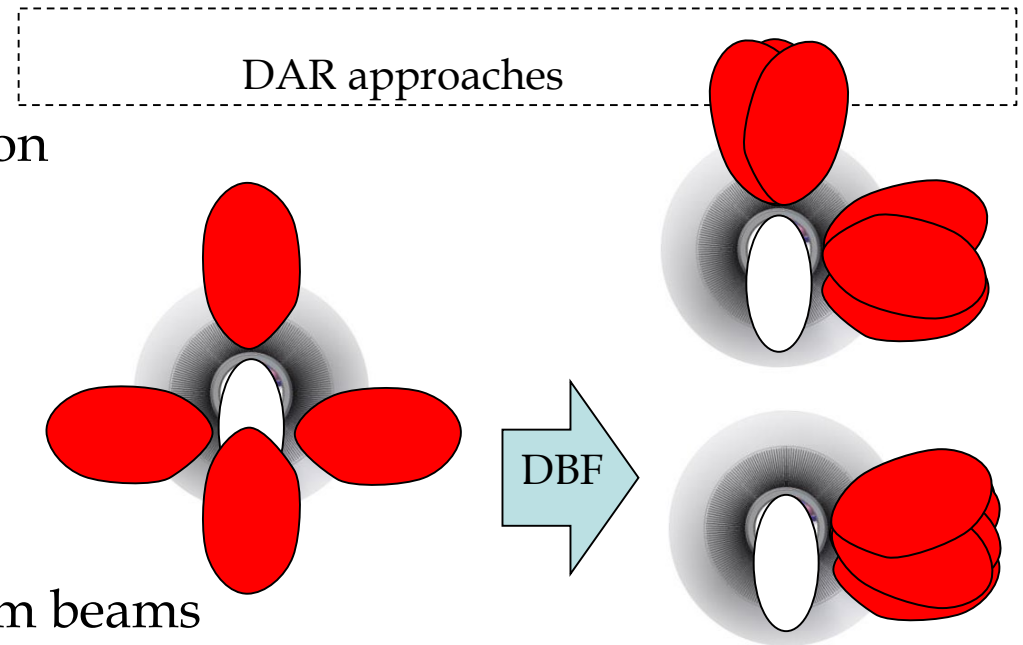
■ Possible strategies in DAR:

Detection:

- for each azimuthal direction
 N_{Σ} sum beams.

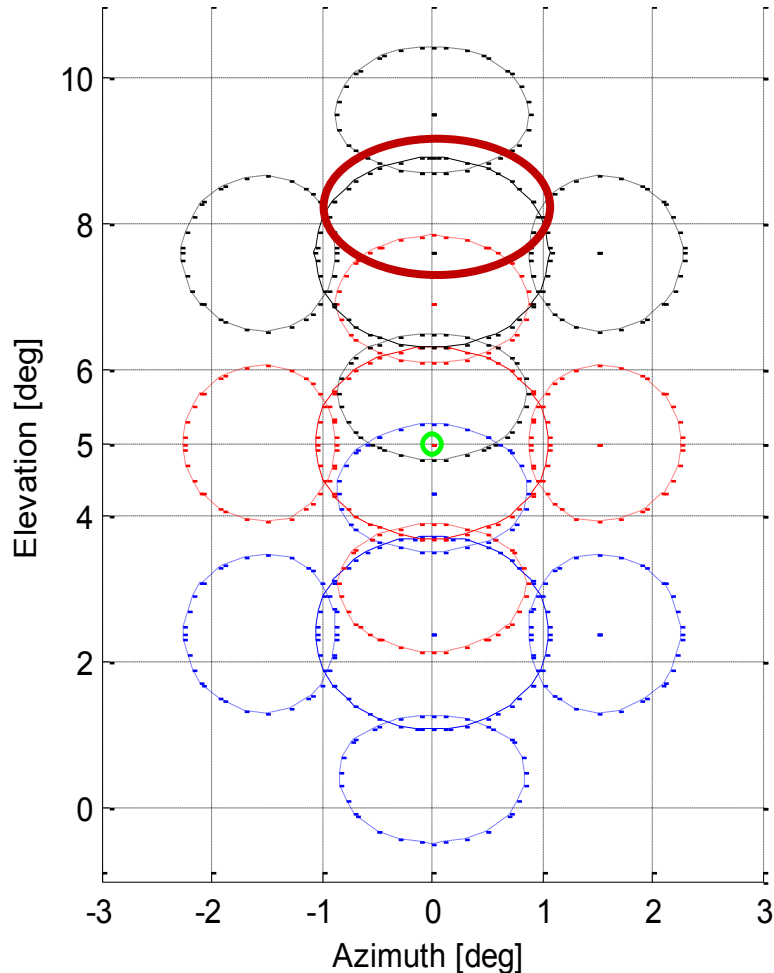
DoA estimation:

- only at DoA and ranges where detections occurred
 - N_{Δ} difference beams.
 - Cluster of crowded sum beams



Detection Beam Cluster for DAR

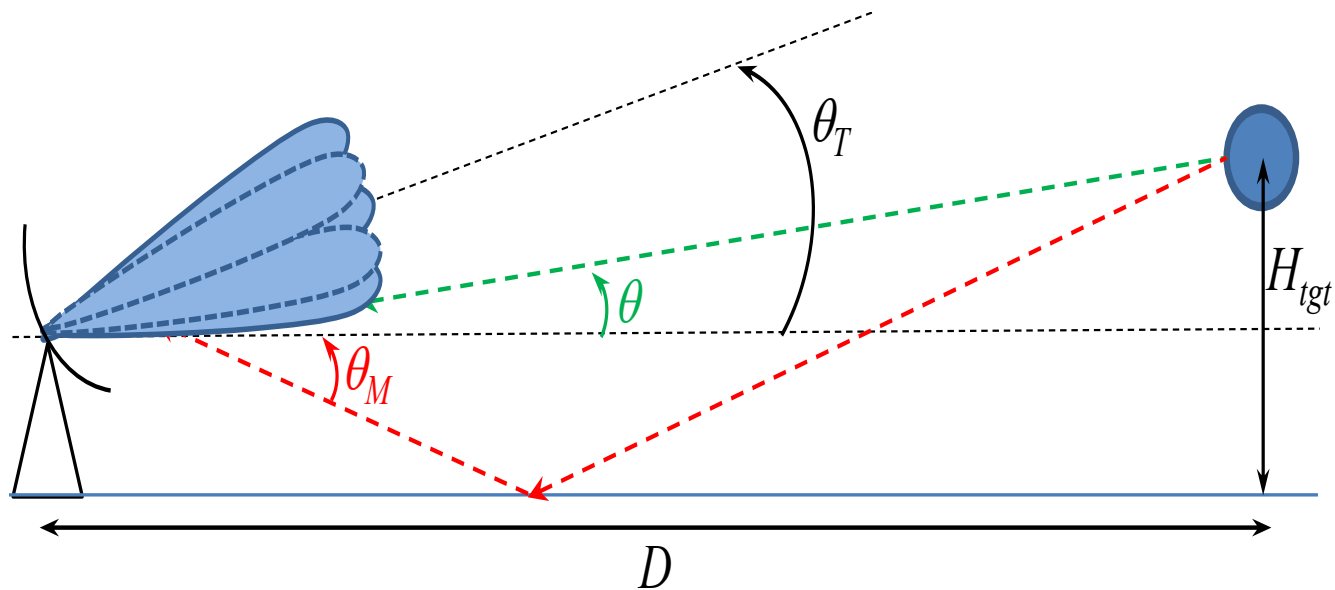
- Beam cluster configuration for radar operating in search mode with low steering direction in elevation (5°).



- Solid lines: sum beams with a width of $2,6^\circ$ in elevation and 2° in azimuth to cover an aperture of nearly 8° in the elevation dimension.
- Dashed lines: difference beams for DoA estimation

Low elevation angles problem (I)

Operational scenario \rightarrow signals from a low altitude target are received through a direct and a specular reflected path in the flat earth model.

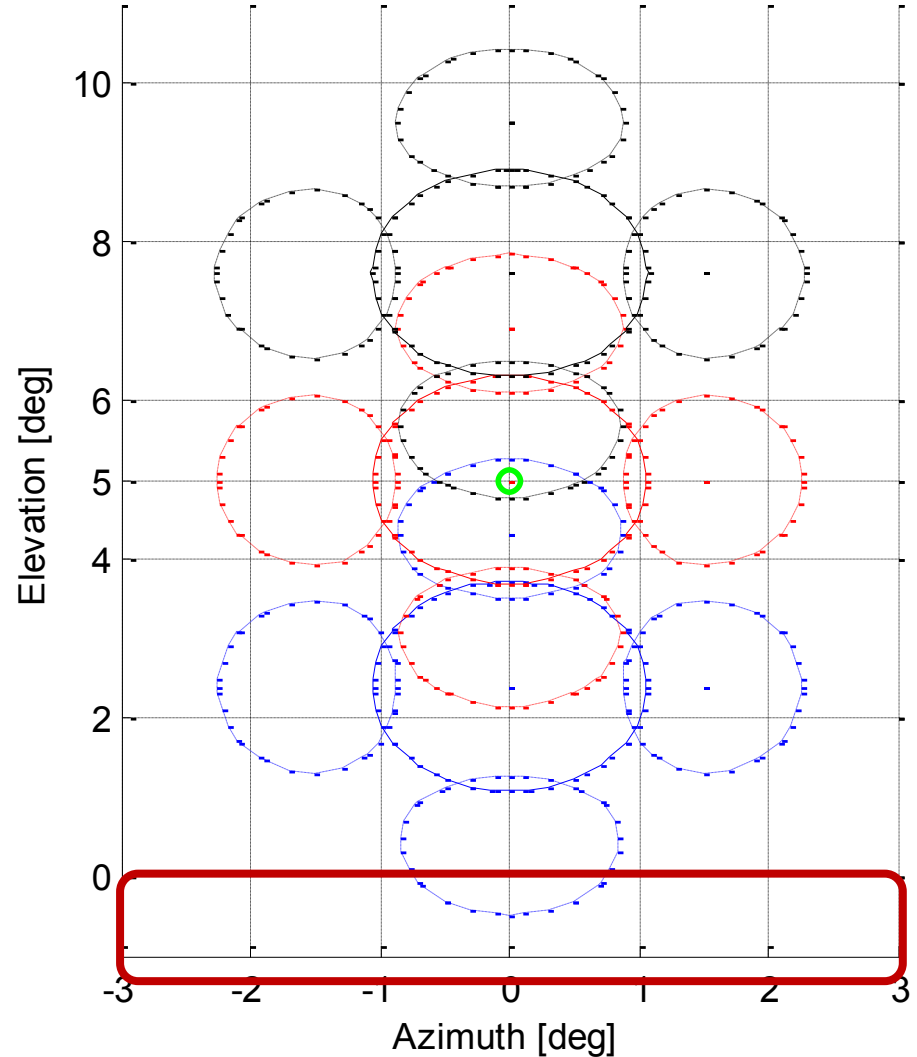


Low elevation angles problem (II)

Lower Sum and especially Difference beams in the cluster may suffer from multipath arising from low-height target.



Possibility of using a different approach for DoA estimation, in particular for the elevation angle.



Presented DoA estimation for DAR

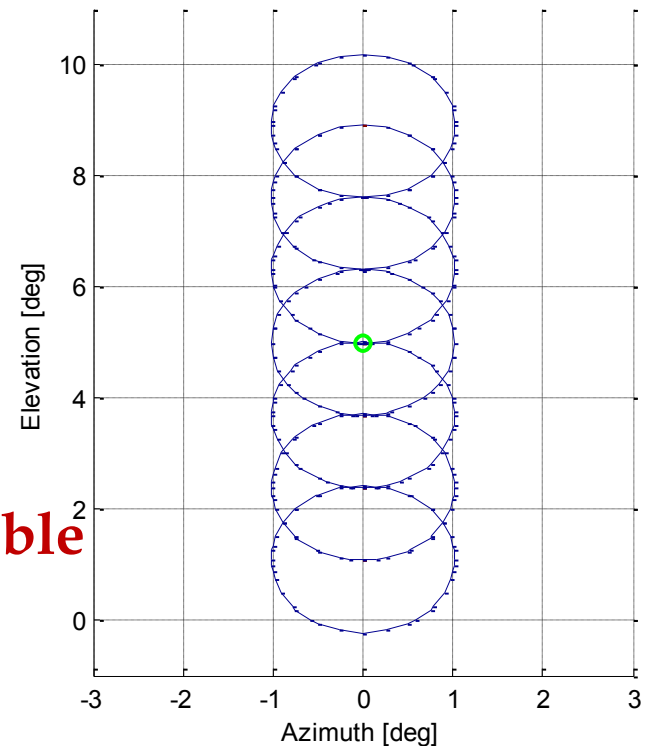
- Data acquired by all elements are available at a central processing unit before beamforming.
- Identification of the beams and resolution cells detections occurred.

Only for those detections a crowded clusters of sum beams properly displaced in the angular area of interest must be formed for accurate angle estimation.



- Use of a wide beam cluster **even a high number of beams is possible for the few detected targets**

Computational cost is certainly low



CRLB derivation for elevation DoA estimation

■ Received signal

$$\mathbf{x}(\theta) = A_0 G_{TX}(\theta, \theta_0) G_E(\theta) \mathbf{T} \mathbf{s}(\theta) + \mathbf{T} \mathbf{n}$$

Steering vector at element level

Transformation matrix from element to cluster of beams

Noise at element level

Element gain

Transmitting gain

■ Probability density function

$$f[\mathbf{x}] = \frac{1}{2\pi \cdot \det(\mathbf{M})} \exp\left\{ -[\mathbf{x} - A_0 \mathbf{v}]^H \mathbf{M}^{-1} [\mathbf{x} - A_0 \mathbf{v}] \right\}$$

Expected value vector

$$\mathbf{M} = \sigma_n^2 \mathbf{T} \mathbf{T}^H$$

Covariance noise matrix at cluster level

■ Elevation DoA estimation accuracy

$$\sigma_\theta^2 = 2 \frac{|A_0|^2}{\sigma_n^2} \dot{\mathbf{v}}^H \left[\mathbf{M}^{-1} - \frac{\mathbf{M}^{-1} \mathbf{v} \mathbf{v}^H \mathbf{M}^{-1}}{\mathbf{v}^H \mathbf{M}^{-1} \mathbf{v}} \right] \dot{\mathbf{v}}$$

Derived expected value vector

Signal to noise ratio at element level

CRLB comparison (I)

- Comparison between the accuracies of monopulse ($3\Sigma+3\Delta$) and estimation of elevation DoA through a cluster of K beams equally spaced in an aperture of 8° .

- **Sum beams**

modified Taylor windows both in azimuth PSLR of 42 dB and elevation PSLR of 36 dB.

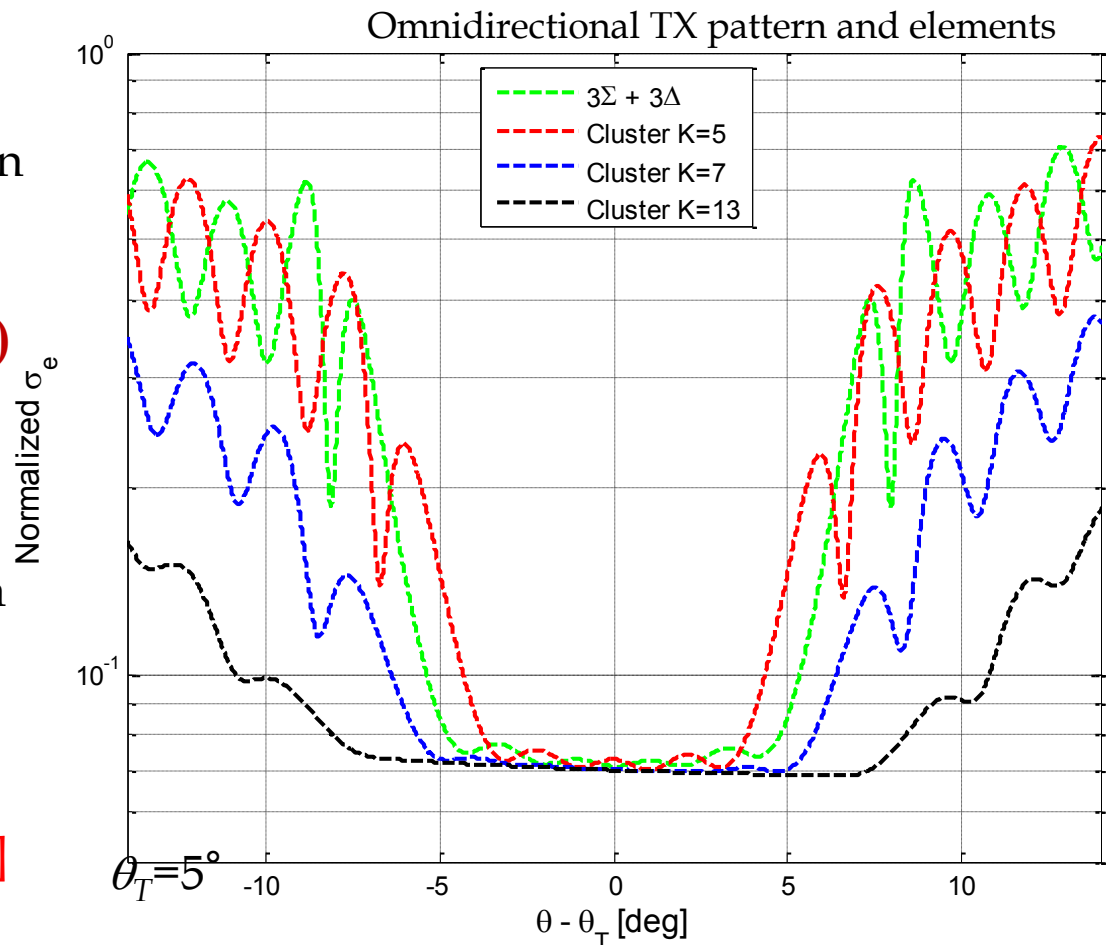
- **Difference beams (elevation)**

Bayliss taper with same PSLR

- $\text{SNR}_{\text{el}} = -20$ dB

→ peak SNR on the central beam of nearly 13 dB.

Performance equivalence, especially in the interval $[-4^\circ, 4^\circ]$



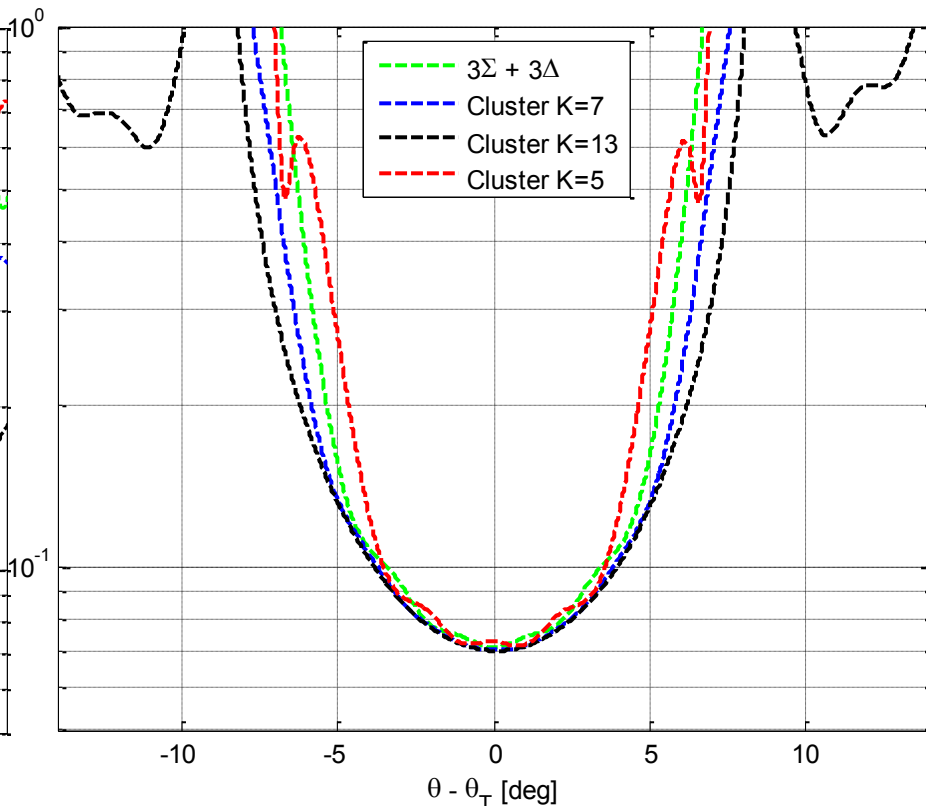
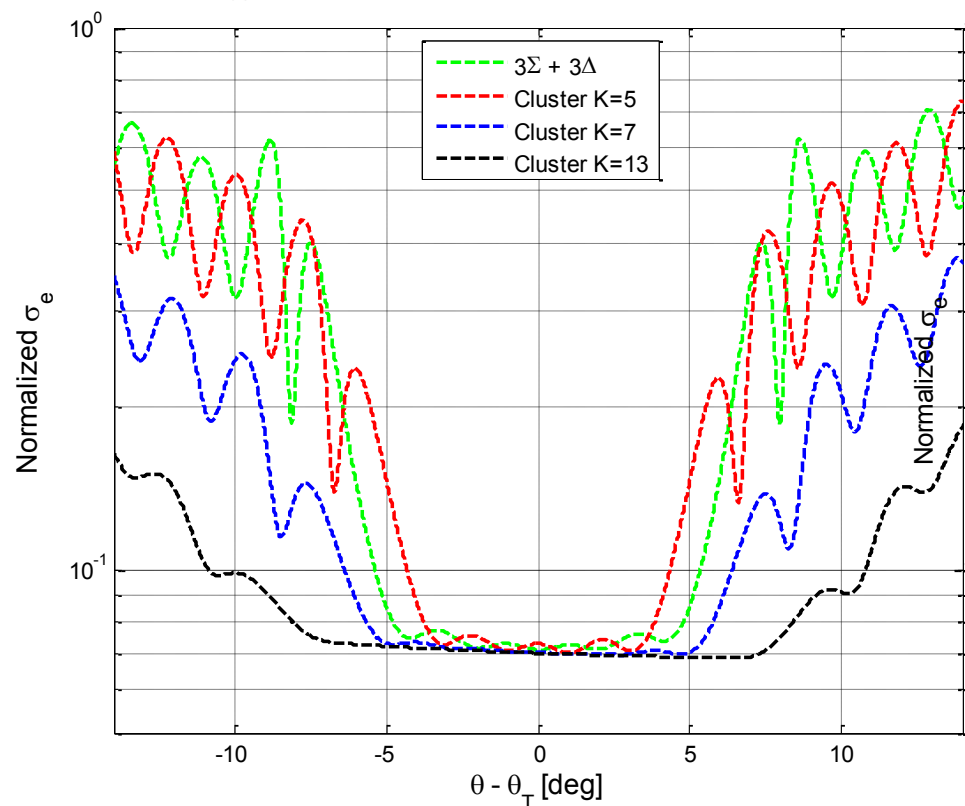
CRLB comparison (II)

Impact of transmit pattern

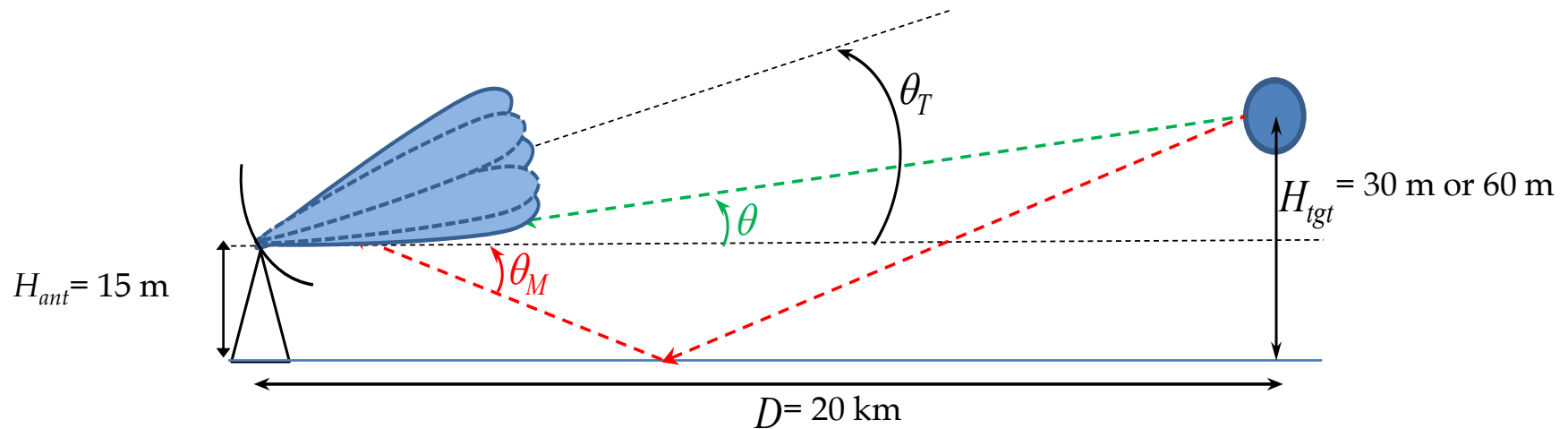
$$\theta_T = 5^\circ$$

Omnidirectional TX pattern and elements

Directive TX pattern and omnidirectional elements



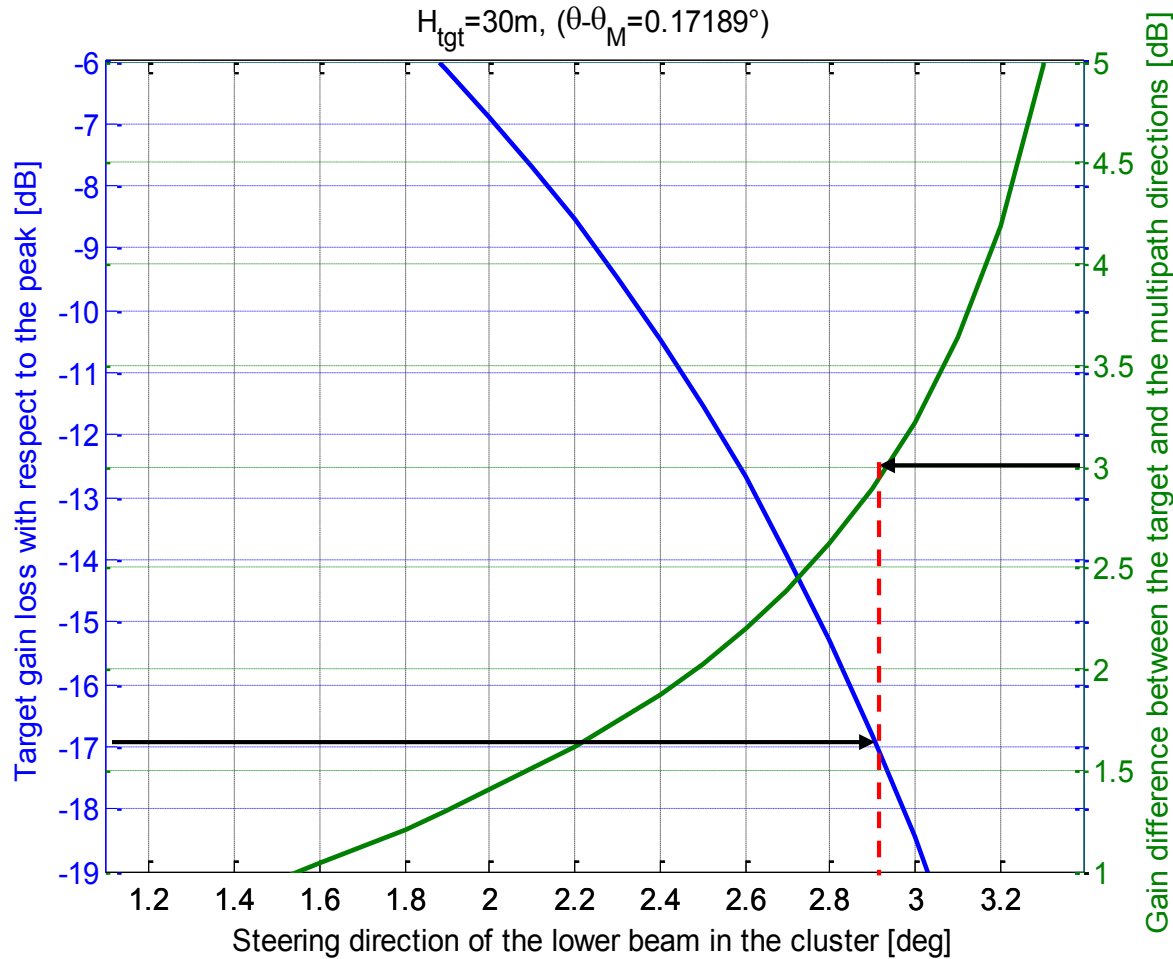
Beam cluster tilt(1/3)



- The steering direction of the lower beam in the cluster is selected
- The steering direction of the remaining beams in the cluster follow it, to uniformly cover the 8° angular aperture.
- AIM: provide a gain of at least X dB to the direct signal from θ with respect to the multipath signal received from θ_M
under worst condition of operation (minimum target height)

Beam cluster tilt (2/3)

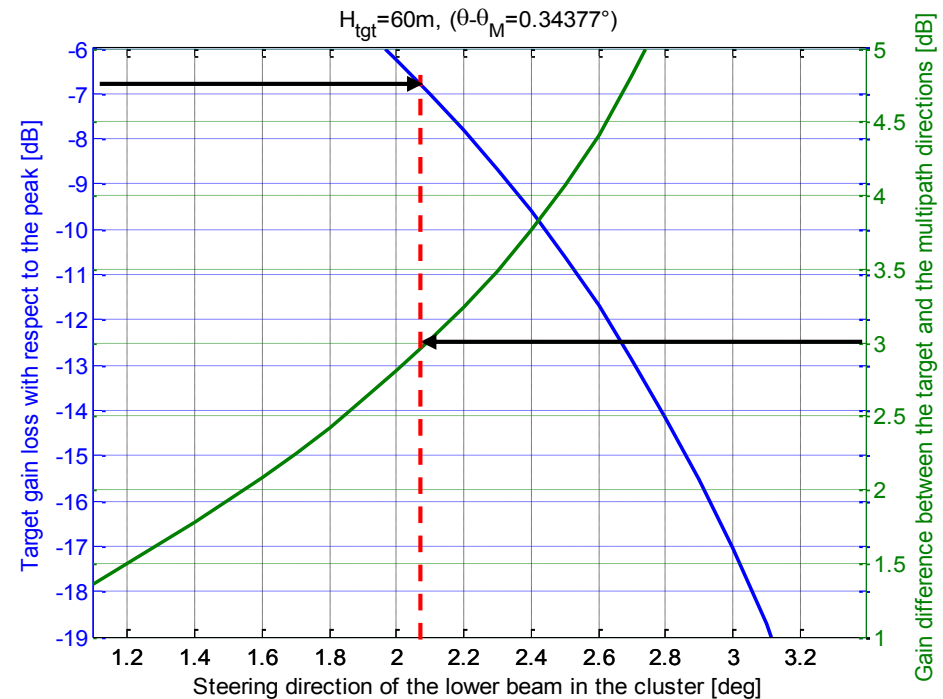
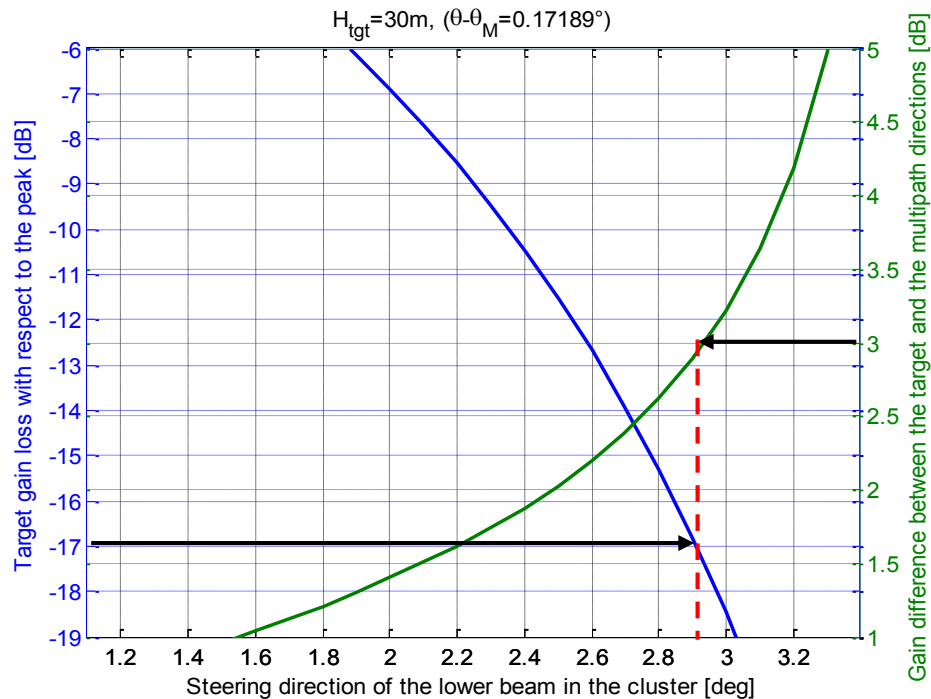
Example: provide a gain of at least 3 dB to the direct signal from θ with respect to the multipath signal received from θ_M



loss of -17 dB
in the target
direction for
 $H_{tgt}=30\text{ m}$

Beam cluster tilt (3/3)

- The design becomes less demanding as the target height increases with a loss of -7 dB in the target direction for $H_{tgt}=60$ m and -17 dB for $H_{tgt}=30$ m.



Conclusions

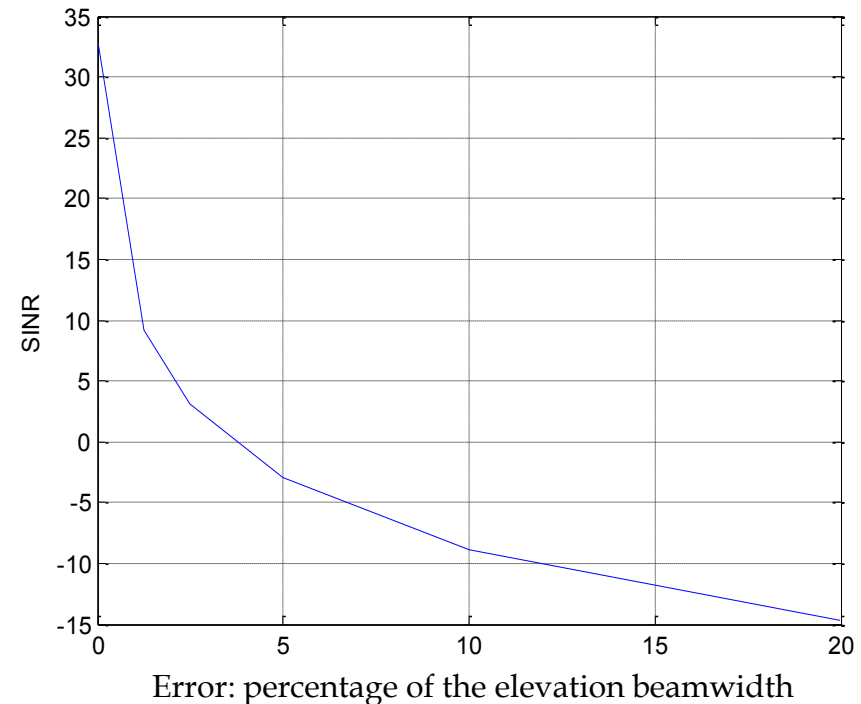
- An innovative conformal DAR has been presented (conical shape factor) with its potentialities and some comparison to more usual PAR
- We derived the theoretical expression of the CRLB for elevation angle estimation using a cluster of beams.
- We analysed the limit performance of DoA estimation achievable with monopulse to those achievable with a RX beam cluster solution that is shown to be more attractive for DAR.
- Performance of both techniques resulted to be comparable, making the second particularly interesting for those situations where monopulse is known to experience performance degradation, as low elevation angle estimation.
- In this latter case an example of the design of the cluster of beams in presence of specular multipath has been provided.

System potentialities: DAR ECCM strategies (1/3)

Approximate knowledge of the jammer DoA

■ Antenna nulling without fast time adaptivity

- ❑ The beam pattern is formed with a null in the known jammer direction without estimating and inverting the disturbance covariance matrix.
- ❑ The accuracy of the knowledge of the jammer DoA has an impact on the achievable Signal to Interference and Noise Ratio (SINR)
- ❑ In the proposed example the beam steering direction is set to $(15^\circ, 0^\circ)$ in elevation and azimuth and the jammer DoA is $(17.5^\circ, 0^\circ)$ and the Jammer to Noise Ratio (JNR) is set to 30 dB
- ❑ The cancellation performance rapidly degrades as the jammer DoA inaccuracy increases

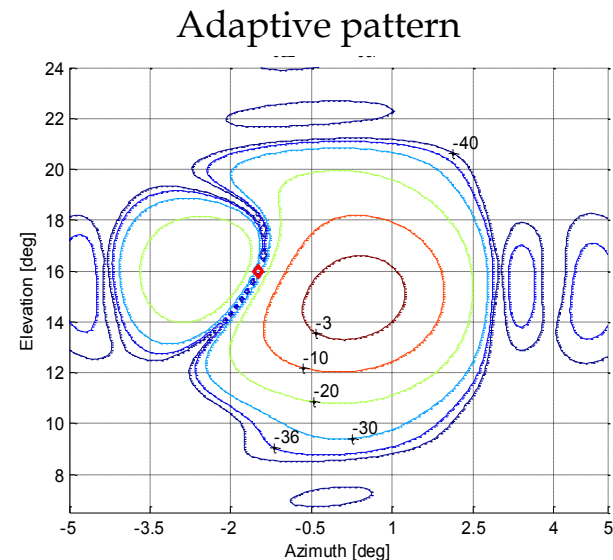
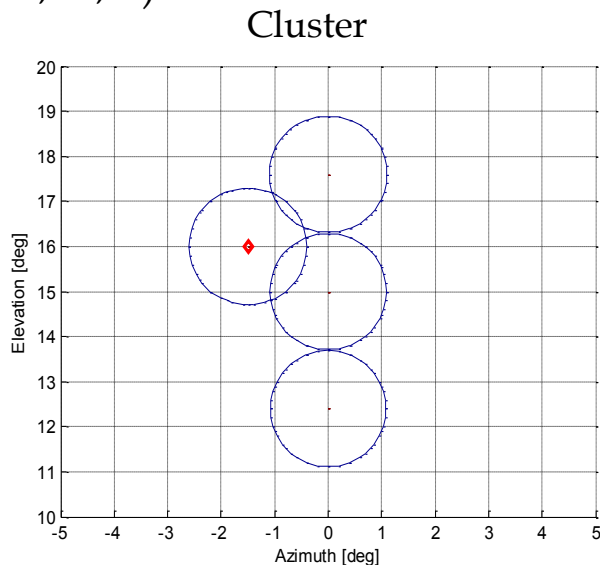


System potentialities: DAR ECCM strategies (2/3)

Approximate knowledge of the jammer DoA

■ Antenna nulling with fast time adaptivity at beam level

- The adaptive beam pattern is formed from a cluster of beams: $N_{\Sigma} + 1$ steered in the estimated jammer direction.
- The covariance matrix to be estimated at beam level has a reduced dimension, still allowing to recover a near ideal performance
- Steering direction is set to $(15^{\circ}, 0^{\circ})$ in elevation and azimuth and the jammer DoA is $(16^{\circ}, -1,5^{\circ})$

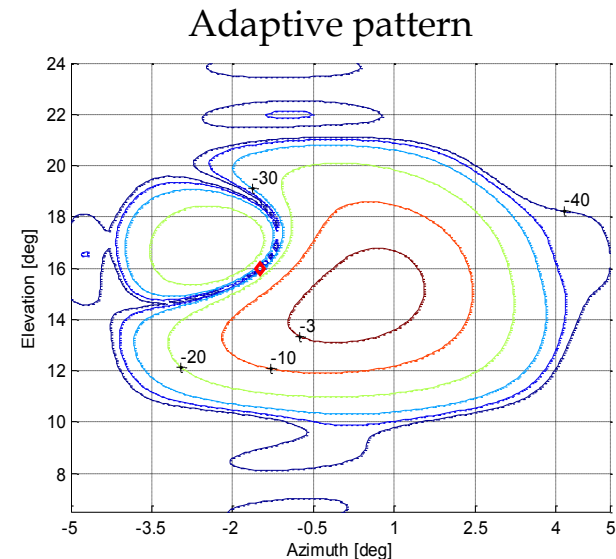
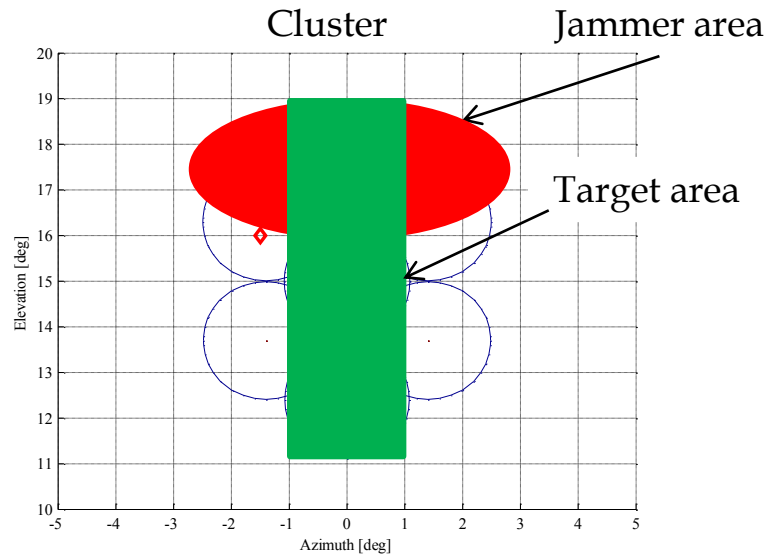


System potentialities: DAR ECCM strategies (3/3)

Jammer DoA not known

■ Antenna nulling with fast time adaptivity at beam level

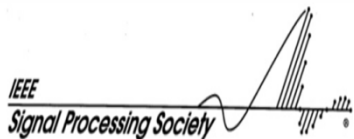
- The adaptive beam pattern is formed from a cluster of sufficient number beams to cover the target and jammer area.
- The covariance matrix to be estimated at beam level has a higher dimension
- Steering direction is set to $(15^\circ, 0^\circ)$ in elevation and azimuth and the jammer DoA is $(16^\circ, -1.5^\circ)$



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